

**UNITED STATES PATENT APPLICATION**

*of*

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**FUEL CELL SYSTEM WITH ACTIVE METHANOL CONCENTRATION  
CONTROL**

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# FUEL CELL SYSTEM WITH ACTIVE METHANOL CONCENTRATION CONTROL

## BACKGROUND OF THE INVENTION

### *Field of the Invention*

5       The present invention relates generally to the field of fuel cells and, more specifically, to a direct methanol fuel cell system in which active control of the concentration of methanol at a critical point within the cell minimizes crossover of methanol through the cell's membrane.

### *Background Information*

10       Fuel cells are devices in which an electrochemical reaction is used to generate electricity. A variety of materials may be suitable for use as a fuel, depending upon the materials chosen for the components of the cell. Organic materials, such as methanol or formaldehyde, are attractive choices for fuels due to their high specific energies.

15       Fuel cell systems may be divided into "reformer based" (*i.e.*, those in which the fuel is processed in some fashion before it is introduced into the cell) or "direct oxidation" in which the fuel is fed directly into the cell without internal processing. Most currently available fuel cell systems are of the reformer-based type and their fuel processing requirement limits their application to relatively large applications relative to a direct oxidation system.

20       An example of the direct oxidation system is the direct methanol fuel cell system or DMFC. In a DMFC, the electrochemical reaction at the anode is a conversion of methanol and water to  $\text{CO}_2$ ,  $\text{H}^+$  and  $\text{e}^-$ . The hydrogen ions flow through a membrane electrolyte to the cathode, while the free electrons flow through a load which is normally

connected between the anode and cathode providing power to the load. At the cathode, oxygen reacts with hydrogen ions and free electrons to form water.

Conventional DMFCs suffer from a problem which is well known to those skilled in the art: cross-over of methanol from the anode to the cathode through the membrane electrolyte, which causes significant loss in efficiency. Cross-over occurs because of the high solubility of methanol in the membrane electrolyte. In order to minimize cross-over, and thereby minimize the loss of efficiency, the concentration of methanol in the fuel feed stream is kept low (*e.g.*, below 1M) by dilution with water. However, dilution of the methanol introduces other disadvantages: (1) the fuel cell's construction becomes more complicated and costly because of the structures and processes needed to store and manage the water; and (2) the energy per unit volume of the fuel cell, which is a critical factor in terms of the fuel cell's potential commercial applications, is reduced.

## SUMMARY OF THE INVENTION

In brief summary, the present invention provides a direct methanol fuel cell system in which, in response to changes in the output power level of the cell, the concentration of methanol supplied to the anode is actively controlled, thereby minimizing methanol cross-over and maintaining efficiency over a wide operating range. Mechanisms for controlling the methanol concentration are preferably constructed using microelectromechanical system (MEMS) fabrication techniques which enable the control mechanism to be readily integrated with the fuel cell's structure.

## BRIEF DESCRIPTION OF THE DRAWINGS

The invention description below refers to the accompanying drawings, of which:  
Fig. 1 is a block diagram of a direct methanol fuel cell known in the prior art;  
Fig. 2 is an exploded view showing details of the internal construction of the fuel cell of Fig. 1;

Fig. 3A is a graph showing the relative concentrations of methanol at various points denoted in Fig. 2;

Fig. 3B is a graph showing the relative concentrations of methanol at various points denoted in Fig. 2 when the fuel cell operates at low and high output power levels;

Fig. 4 is a block diagram of a direct methanol fuel cell system that includes active methanol concentration control constructed in accordance with a preferred embodiment of the present invention;

Fig. 5 is a diagram of a methanol concentration regulator constructed using MEMS fabrication techniques in accordance with one embodiment of the present invention;

Fig. 6 is a diagram of a methanol concentration regulator constructed using MEMS fabrication techniques in accordance with an alternative embodiment of the present invention; and

Fig. 7 is a block diagram of an alternative embodiment of the present invention in which active methanol concentration control is provided without an output power detector.

## DETAILED DESCRIPTION OF AN ILLUSTRATIVE EMBODIMENT

Figure 1 shows a conventional direct methanol fuel cell 2 in which a housing 4 encloses a cathode 6, a membrane electrolyte 8 and an anode 10. A load 12 is connected across cathode 6 and anode 10. Methanol and water are introduced into the anode side of housing 4 while oxygen is introduced into the cathode side of the housing. The source of the oxygen is preferably ambient air, but it should be understood that other sources could be used. As a result of the reactions at the anode and cathode, free electrons flow from anode 10 through load 12 to cathode 6, while hydrogen ions flow from anode 10 through membrane electrolyte 8 to cathode 6. So long as the reactions continue, a current is maintained through load 12.

Figure 2 illustrates certain details the internal construction of anode 10, the components of which are shown in exploded form for enhanced clarity. One face of a flow plate 14 is formed as a series of grooves or channels 22a through which a methanol-water mixture (not shown) passes. Flow plate 14 is normally in direct contact with one face of

a gas diffusion layer (GDL) 16. The opposite face of GDL 16 is in direct contact with one face of an electrode 18. Similarly, the opposite face of electrode 18 is in direct contact with one side of membrane electrolyte 8. Four points of interest within anode 10 are denoted by the reference letters A, B, C and D, respectively. Points A, B and C represent interfaces between components and point D represents the cathode side of membrane electrolyte 8.

Referring now to Figures 2 and 3A, one may see how the concentration of methanol varies at points A-D under certain operating conditions. Figure 3A shows methanol concentrations for a typical DMFC operating at a particular output power level. As may be expected, the methanol concentration is highest at point A (*i.e.*, the interface between flow plate 14 and GDL 16) and lowest at point D, with a significant reduction in concentration caused by the electrode 18. While the methanol concentration at point D is low, it is not zero, meaning that some methanol has crossed-over membrane electrolyte 8 and reached the cathode indicating that some methanol has passed through the membrane electrolyte without supplying current to the load.

Referring now to Figure 3B, relative methanol concentrations at points A-D are shown for a fuel cell operating at a low output power level, denoted by reference numeral 24, and at a high power level, denoted by reference numeral 26. In the low power case, the methanol concentration at point C is significantly elevated, indicating excessive methanol cross-over and attendant loss of efficiency. In the high power case, the methanol concentration at point D is quite low, suggesting that an optimal amount or possibly insufficient methanol is being supplied to electrode 18.

Figure 4 shows a DMFC system 28 constructed in accordance a preferred embodiment of the present invention. A housing 30 encloses a cathode 32, membrane electrolyte 34, anode 36, a methanol concentration regulator 38 and an output power detector 40. Detector 40 functions to detect the output power level of system 28 and produce a signal (or other suitable indicator) indicative of changes in that power level to concentration regulator 38. In response to changes in the output power level, concentration regulator 38 functions to increase or decrease the concentration of methanol supplied to anode

36 such that methanol cross-over at membrane electrolyte 34 and the associated loss in efficiency are substantially minimized.

System 20 may be constructed from a variety of commercially-available materials using MEMS fabrication techniques, conventional techniques, or a combination of both.

5 Figure 5 shows a preferred embodiment of methanol concentration regulator 38 in which the regulator is constructed as an actuator using MEMS fabrication techniques. A closed chamber 44 which is filled with a control liquid 46 may be secured to or formed integrally with flow plate 14 (Fig. 2). A resistive element 48 is disposed within liquid 46 and coupled to power detector 40. As resistive element 48 heats liquid 46, pressure is  
10 exerted on flow plate 14, GDL 16 and electrode 18, thereby reducing the flow of methanol to anode 8. Conversely, as element 48 cools, pressure is reduced and the concentration of methanol supplied to anode 8 increases.

Figure 6 shows an alternative embodiment of methanol concentration regulator 38. Here, a microactuator 50, which is preferably constructed using MEMS fabrication  
15 techniques, is located either proximate to or possibly within channel 22a of flow plate 14. Thus, as microactuator 50 operates, it functions to apply pressure to or reduced the cross-section of channel 22a, thereby restricting the flow of methanol through it.

Figure 7 shows an alternative embodiment of a DMFC system with active methanol concentration control. Components which are comparable to those shown in Figure 4  
20 are assigned like reference numbers. A methanol concentration regulator 52 is connected in series with load 42. In this embodiment, the output power detector has been eliminated as a discrete component, and its function is effectively integrated into the regulator. Regulator 52 is preferably implemented using a microactuator which may be constructed using a any of a variety of techniques, as described above, with an appropriate choice of  
25 material based on the expected power range for a particular application. Regulator 52, responsive to changes in potential at anode 36 or load level, operates to vary the concentration of methanol provided to the anode.

It should be understood by those skilled in the art that various other structures and techniques may be used to implement methanol concentration regulator 38, particularly

those which change the porosity or tortuosity of GDL 16 or electrode 18 or both. Regulator 38 may be mechanically coupled to or integrated with either anode 8 or GDL 16. It should also be understood that the present invention may be used with fuels other than methanol/water mixtures.

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What is claimed is: